

A Nobel Smart Antenna for Broad-Band Applications

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ABSTRACT

In this research paper a short review on smart antenna is presented. The smart antenna consisting of micro strip patches array has been presented. It will enable a higher capacity in wireless networks by effectively reducing multipath and co-channel interference. This is achieved by focusing the radiation only in the desired direction and adjusting itself to changing or signal environment. A Nobel technique is investigated to form the desired shape forming of beam. This has become a part of range improvement and increase in capacity of smart antenna.

Key words: Smart antenna, Micro strip patch arrays, Range improvement.

INTRODUCTION

Smart antennas are antennas arrays that are combined with signals processing in space and real time. Such antennas have their special need in cellular and mobile communication systems. The smart antennas have the properties of increasing the spectrum efficiency, channel capacity and coverage range. They have ability to provide certain channel in certain direction. They are able to reduce the propagation problems such as multipath fading, co-channel interference and have capacity to improve communication indices¹⁻³. The smart antennas are characterized as adaptive array antennas, intelligent antennas, spatial processing and digital beam forming antennas. Mainly there are two types of smart antennas, the switched beam smart antenna and adaptive arrays smart antennas. The switched beam smart antenna divides the communication area into micro sectors. Each micro sector contains a predetermined fixed beam pattern. The adaptive system dynamically alters the pattern to optimized communication performance^{4,5}. The adaptive array theory is based on optimization method and on real time response in a transit environment. Smart antennas can be analyzed for different network topology and mobility scenario. Their geometry is analyzed with appropriate feed network and algorithms for fast beam forming and

direction of arrival. The cost of smart antennas continues to be the most critical issues.

The early smart antenna systems were designed for use in military applications to suppress interfering or jamming signals from the enemy⁶. Since interference suppression was a feature in this system, this technology was borrowed to apply to personal wireless communications where interference was limiting the numbers of users that a network could handle. It is major challenge to apply smart antenna technology to personal wireless communications since traffic is denser. Also, the time available for complex computations is limited. However, the advent of powerful, low-cost, digital processing components and the development of software-based techniques has made smart antenna systems practical reality for cellular communications systems.

Basic working mechanism

A smart antenna system can perform the following functions: first the direction of arrival of all the incoming signals including the interfering signals and the multipath signals are estimated using the direction of Arrival algorithms. Secondly, the desired user signal is identified and separated from the rest of unwanted incoming signals. Lastly a beam is steered in the direction of desired signal

and the user is tracked as he moves while placing nulls at interfering signal directions by constantly updating complex weights.

It is quite evident that the direction of radiation of the main beam in the array depends upon the phase difference between the elements of the array. Therefore, it is possible to continuously steer the main beam in any direction by adjusting the progressive phase difference $\hat{\alpha}$ between the elements. The same concept forms the basis in adaptive array systems in which the phase is adjusted to achieve maximum radiation in the desired direction.

In a beam forming network typically the signals incident at the individual elements are combined intelligently to form a single desired beam formed output. Before the incoming signals are weighted they are brought down the baseband or intermediate frequencies (IF's). The receivers provided at the output of each element perform the necessary frequency down conversion. Adaptive antenna array systems use digital signal processors (DSP's) to weight the incoming signal. Therefore, it is required that the down-converted signal can be converted into digital format before they are processed by DSP. Analog to digital converters (ADC's) are provided for this purpose. For accurate performance, they are required to provide accurate translation of the RF signal from the analog to digital domain. The digital signal processors form the heart of the system, which accepts the IF signal in digital format and the processing of digital data is driven by software. The processor interprets the incoming data information, determines the complex weights (amplification and phase information) and multiplies the weights to each element output to optimize the array pattern. The optimization is based on a particular criterion, which minimizes the contribution from noise and interference while producing maximum beam gain at the desired direction. There are several algorithms based on different criteria for updating and computing the optimum weights. Many methods have been proposed to achieve phase shifting without an electronic phase shifter, namely: Electromechanical tuning method using a piezoelectric transducer (PET)⁶; Beam steering by means of a coupled-oscillator technique², Optical beam forming networks Based on liquid crystal

phase shifters; Optical techniques for beam steering by ferrite-based Patch arrays⁷⁻⁹ For the application of semi-smart antennas to achieve beam steering in real-time, a novel phase-Shifting method is presented. By non-mechanically adjusting the value of the effective dielectric Constant of the length of the dielectric plates, it is possible to perform beam steering without Employing methods of digital phase shifting. This permits simpler construction and lower costs. The structures were simulated using the commercial software, Ansoft HFSS Element methods(FEM)

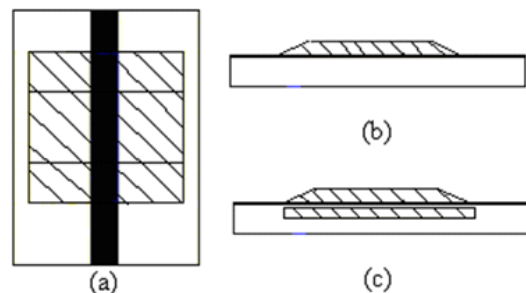


Fig. 1.

Simulations of Transmission Line Phase Shifting with Dielectric Plates

The first is with a single-layer dielectric plate attached to the transmission line, as shown in Fig.1(b); the second is with a dual-layer combination of dielectric plate, both attached to, and 0.1mm under, the transmission line, as shown in Fig.1(c). The edge of the upper dielectric plate is tapered to suppress the reflection loss. The substrate has a permittivity of 4.0 F/m and dimensions of $(40 \times 12 \times 2) \text{ mm}^3$. The width of the transmission line is 2mm. The dimensions of the dielectric plate is $(L \times 10 \times 1) \text{ mm}^3$, where $0 < L < 30 \text{ mm}$. Fig.2 shows the phase of S_{21} simulated with single-layer dielectric plate. Fig.5 shows the phase of S_{-21} simulated with a dual-layer of dielectric plates. Clearly, phase shift can be seen introduced by using a single-layer dielectric plate or a dual-layer of dielectric plates. It is noticeable that phase increases with the increase in the effective permittivity as well as with the increase in length of the dielectric plate. The dual-layer structure produces a more evident phase shift, of which the phase shift has increased nearly 66.7% (when $L=5 \text{ mm}$, 107.7% (when $L=20 \text{ mm}$, and 115.9% (when

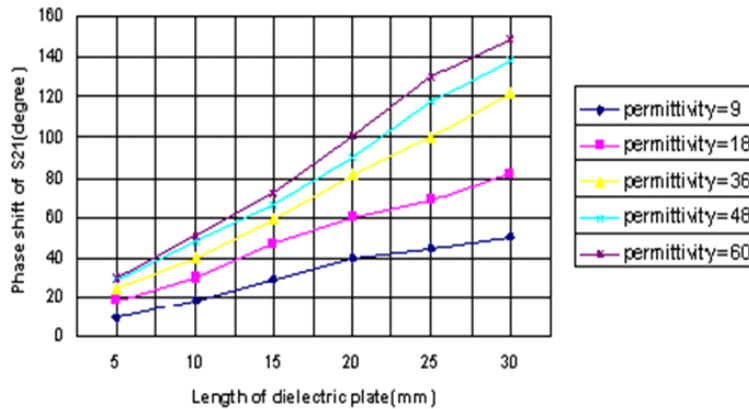


Fig. 2:

\bar{R}_{xx}

L=30mm,) respectively, comparing to single-layer structure. This is attributed to a Heavier attenuation of the propagation constant.

Array Correlation Matrix

Many of the AOA algorithms rely on the array correlation matrix. In order to understand

The array correlation matrix. Let us begin with a description of the array, the received signal, and the additive noise. Figure (4) depicts an array with incident plane waves from various directions. It also shows D signals arriving from D directions. They are received by an array of M elements with M potential weights

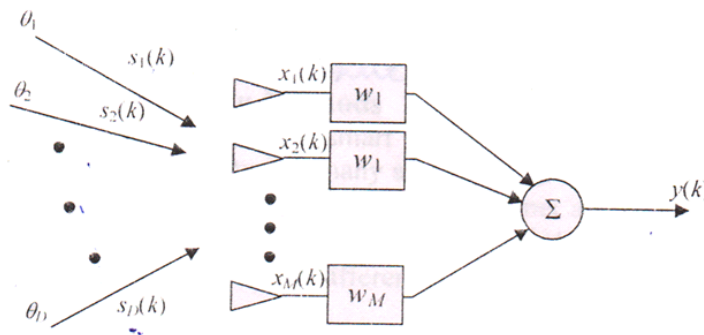


Fig. 3:

Each received signal $x_m(k)$ includes additive white Gaussian noise with mean zero. Time is represented by the k th time sample. Thus, the array output y can be given in the following form:

$$y(k) = \bar{w}^T \cdot \bar{x}(k) \quad \dots(1)$$

Where $\bar{x} = \bar{A} \cdot \bar{s}(k) + \bar{n}(k)$ And $\bar{w} = [w_1 w_2 \dots w_M]^T$ = array weights $\dots(2)$

- $\bar{s}(k)$ = vector of incident complex monochromatic signals at time k
- $\bar{n}(k)$ = noise vector at each array element m , zero mean, variance σ_n^2
- $\bar{a}(\theta_i)$ = Element array steering vector for the (θ_i) direction of arrival
- $\bar{A} = [\bar{a}(\theta_1) \bar{a}(\theta_2) \dots \bar{a}(\theta_D)]$ is an $M \times D$ matrix of steering vectors.

The D -complex signals arrive at angles θ_i and are intercepted by the M antenna elements. It is initially assumed that the arriving signals are monochromatic and the number of arriving signals $D < M$. It is understood that the arriving signals are

time varying and thus our calculations are based upon time snapshots of the incoming signal. Obviously if the transmitters are moving, the matrix of steering vectors is changing with time and the corresponding arrival angles are changing, unless otherwise stated, the time dependence will be suppressed in Eqs. (1) & (2). In order to simplify the notation let us define the M X M array correlation matrix \bar{R}_{xx} as

$$\bar{R}_{xx} = E[\bar{x} \cdot \bar{x}^H] = \bar{A}\bar{R}_{ss}\bar{A}^H + \bar{R}_{nn} \quad \dots(3)$$

Where: $E[\bar{x} \cdot \bar{x}^H]$ is the expected value =

$\bar{R}_{xx} = D X D$ source correlation matrix

$\bar{R}_{nn} = \sigma_n^2 \bar{I} = M X M$ noise correlation matrix,

$\bar{I} = N X N$ identity matrix

H_{superscript} is the Hermitian operator (transpose complex conjugate)

The exact statistics for the noise and signals are unknown, but we can assume that the process is ergodic. In that case the correlation can be approximated by the use of a time- averaged correlation. In that case the correlation matrices are defined by

$$\hat{R}_{xx} \approx \frac{1}{K} \sum_{k=1}^K \bar{x}(k) \bar{x}^H(k), \hat{R}_{ss} \approx \frac{1}{K} \sum_{k=1}^K \bar{s}(k) \bar{s}^H(k), \hat{R}_{nn} \approx \frac{1}{K} \sum_{k=1}^K \bar{n}(k) \bar{n}^H(k) \quad \dots(4)$$

Where K is the number of snapshots. The goal of AOA estimation techniques is to define a

function that gives an indication of the angles of arrival based upon maxima vs. angle. This function is traditionally called pseudospectrum $P(\theta)$ and the units can be in energy or in watts .

The exponential growth of wireless communications system and the limited bandwidth available for those systems has created problems which all wireless providers are working to solve. One potential solution to the bandwidth limitation is the use of smart antenna systems. The demand for increased capacity in wireless networks motivated recent research to ward wireless systems that exploit space selectivity. As a result there are many efforts devoted to the design of smart antenna arrays. The term smart implies the use of signal processing in order to shape the beam pattern according to certain conditions. For an array to be Smart implies sophistication beyond merely steering the beam to a direction of interest. Smart essentially means computer control of the antenna performance. Smart antennas hold the promise for improved radar system, improved system capacities with mobile wireless, and improved access.

CONCLUSIONS

To acquire the desired radiation pattern from the base station following negotiation, a novel micro-strip phased-array antenna with single layer or dual layer dielectric plates may be employed. The dielectric plates are designed to work as phase-shifters between the elements of the array. By non-mechanically adjusting the value of the effective dielectric constant or the length of the dielectric plates, it is possible to perform the beam steering without employing methods of digital phase shifting. This affords simpler construction and lower costs.

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