

Heating of a Finite Slab with CW Laser in Relation to Cooling Conditions- at the Rear Surface

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ABSTRACT

Heating a slab induced by laser irradiance is studied. The heat diffusion equation is solved using the Laplace integral transform method. The critical time t_m required to initiate melting is obtained for the elements: Aluminum (Al), Gold (Au), Germanium (Ge) and Silicon (Si). Good cooling conditions at the rear surface of the slab are assumed. The obtained results show that for the considered elements and for such sources of high power density, cooling conditions at the rear surface are not of pronouncing effect. The effect of laser power density on the critical time required to initiate melting is predominant.

Keywords: Laser heating, Laser damage, Heat diffusion equation, Laplace transform.

INTRODUCTION

Laser heating of materials has aroused considerable interest¹⁻²³ due to its demonstrated importance in many processes for industrial applications such as spot welding, scribing and hole drilling, optical recording, semiconductor materials processing.

Serious trials are made to solve the diffusion equation describing the heating problem subjected to different boundary and initial conditions. The bulk of such trials have been numerically based. Some attempts are treated analytically¹²⁻²³.

The present treatment represents one of such analytical trials oriented to study the problem of heating a slab considering the cooling conditions at its rear surface using Laplace integral transform technique.

irradiance q_0 (W/m²) incident on the front surface and perpendicular to it. The diameter of the laser beam is assumed to be large compared to the thermal penetration depth within the slab, and thus the problem is solved as a one-dimensional problem¹. The thermal and optical properties are assumed to be temperature independent.

The heat-flow equation for the temperature rise $T(x,t)$ has the form :

$$\frac{\partial T(x,t)}{\partial t} = \alpha \frac{\partial^2 T(x,t)}{\partial x^2}, \quad x \geq 0, \quad t > 0 \dots(1)$$

where $T(x,t)$ is the excess temperature with respect to the ambient temperature T_0 , $\alpha = \lambda/\rho C_p$ is the thermal diffusion coefficient of the slab in terms of the thermal conductivity λ and the heat capacity per unit volume (ρC_p). Eq. (1) is subjected to the initial condition :

$$T(x,0) = 0 \dots(2)$$

Theory

In setting up the problem it is assumed that the slab is subjected to a constant flux of laser

And the boundary conditions :

i. At the front surface $-\lambda \frac{\partial T}{\partial x} \bigg|_{x=0} = q_0 A \dots (3)$

ii. At the rear surface ($x = d$)

$$\int_0^d q_0 A dx = \int_0^d \rho C_p T(x,t) dx + \int_0^d h T(d,t) dx \dots (4)$$

where, A is the optical absorptance at the front surface.

i. $1 > \beta \geq 0 \dots (16)$

and ii. $1 > a \coth \sqrt{s/\alpha} d \geq 0 \dots (17)$

Derivation of the required solution

The Laplace transform of equation (1) with respect to the time variable "t" gives :

$$s \bar{T}(x,s) - T(x,0) = \alpha \frac{\partial^2}{\partial x^2} \bar{T}(x,s) \dots (5)$$

where $\bar{T}(x,s)$ is the Laplace transform of $T(x,t)$.

One must also write the Laplace transform of the initial and boundary conditions this gives :

i. $\bar{T}(x,0) = 0 \dots (6)$

ii. $-\lambda \frac{\partial}{\partial x} \bar{T}(0,s) = \frac{q_0 A}{s} \dots (7)$

$$iii \frac{q_0 A}{s^2} = \int_0^d \rho C_p \bar{T}(x,s) dx + \int_0^d h \bar{T}(d,s) dx \dots (8)$$

Substituting equation (2) into equation (5)

gives :

$$s \bar{T}(x,s) = \alpha \frac{\partial^2 \bar{T}(x,s)}{\partial x^2} \dots (9)$$

The solution of equation (9) can be written in the form :

$$T(x,s) = c_1 \exp(+\sqrt{s/\alpha} x) + c_2 \exp(-\sqrt{s/\alpha} x) \dots (10)$$

Applying the conditions (6-8) to equation (10) one gets :

$$-\lambda \sqrt{s/\alpha} (c_1 - c_2) = \frac{q_0 A}{s} \dots (11)$$

One can determine the values of c_1 and c_2 .

The solution can finally be written in the form.

$$\bar{T}(x,s) = F(s) \left\{ \frac{1 + a \tanh \sqrt{s/\alpha} (d-x)}{1 + a \coth \sqrt{s/\alpha} d} \right\} = F(s) (1 - \beta) \dots (12)$$

Table 1: The physical and optical properties of the chosen elements

Element	ρ Kg/m ³	λ W/mK	α m ² /s	C_p J/kgK	A_1	T_m (K)
Aluminium	2700	238	8.41E-5	893	0.056	636
Gold	19320	315	6.50E-5	251	0.014	1037
Germanium	5324	59	3.50E-5	315	0.678	1209
Silicon	2328	168	8.50E-5	715	0.678[28]	1685

Table 2: The critical time t_m required to initiate melting

Element	$q, 1E12$ W/m ² $t_m, h=0$	$q, 1E12$ W/m ² $t_m, h=10^5$	$q, 1E14$ W/m ² $t_m, h=0$	$q, 1E14$ W/m ² $t_m, h=10^5$
Aluminium	162,ns	162,ns	1.58,ns	1.58,ns
Gold	1.82 μ s 1.67 μ s[19]	1.82 μ s	18.10,ns	18.10,ns
Germanium	15.20,ns	15.20,ns	0.095,ns	0.095,ns
Silicon	25,ns	25,ns	0.224,ns	0.224,ns

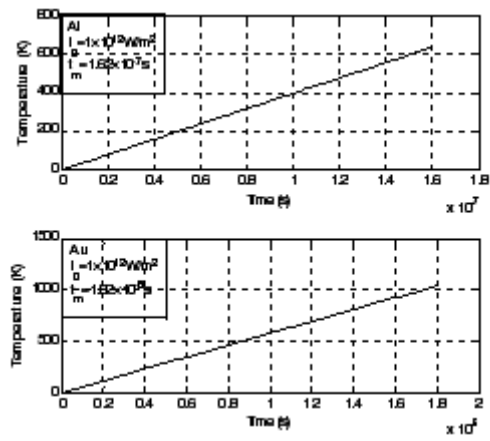
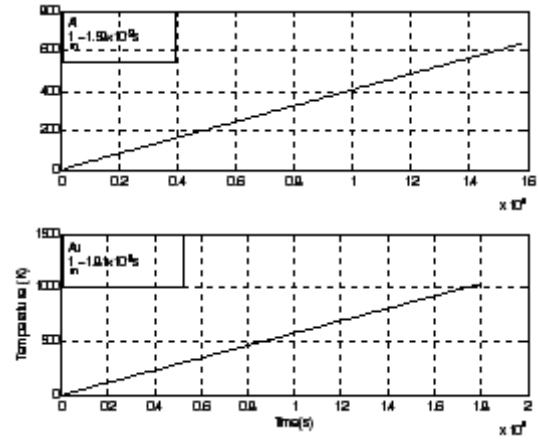
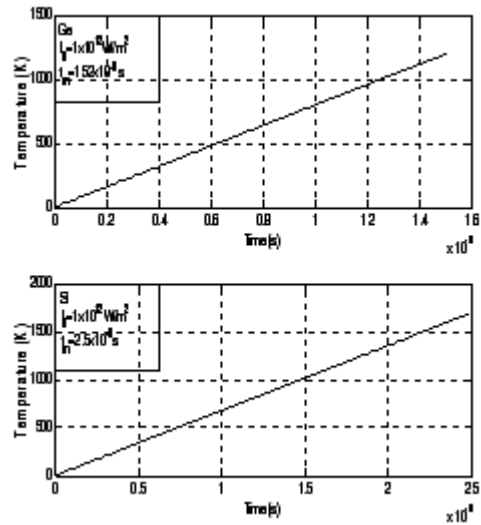
Fig. 1: $q=1\text{E}12\text{W/m}^2$ Fig. 2: $q=1\text{E}14 \text{ w/m}^2$ 

Fig. 3:

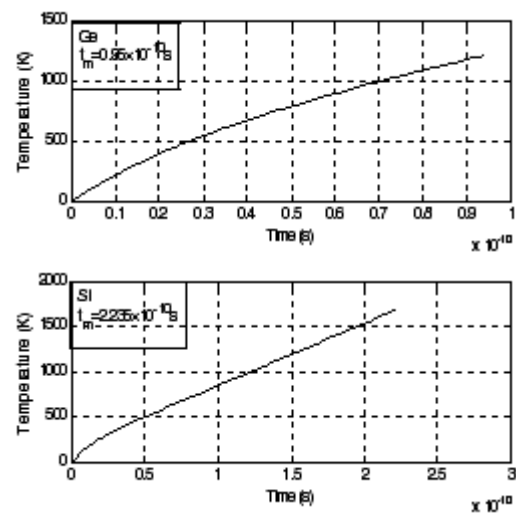
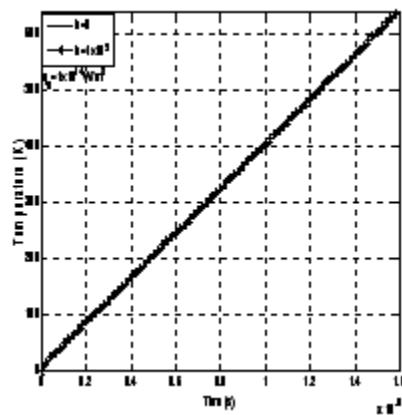
Fig. 4: $q=1\text{E}14 \text{ w/m}^2$ 

Fig. 5: Al

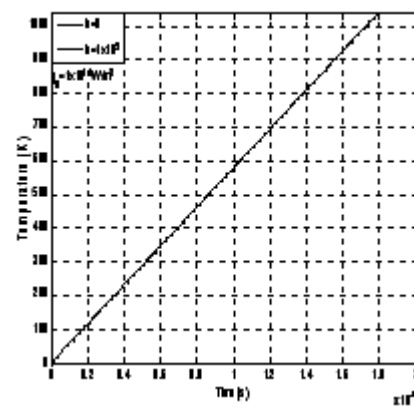


Fig. 6: Gold

Where

$$F(s) = \frac{q_0 A \cosh \sqrt{s/\alpha} (d-x)}{\lambda s \sqrt{s/\alpha} \sinh \sqrt{s/\alpha} d} \quad \dots(13)$$

$$a = h/\lambda \sqrt{s/\alpha}, \quad \dots(14)$$

$$\beta = \frac{a \left\{ \coth \sqrt{s/\alpha} d - \tanh \sqrt{s/\alpha} (d-x) \right\}}{\left\{ 1 + a \coth \sqrt{s/\alpha} d \right\}} \quad \dots(15)$$

It is worth noting that for positive arguments the hyperbolic functions $\coth(x)$ and $\tanh(x)$ are positive. Moreover, as x increases from zero to $+\infty$, $\tanh(x)$ increases from 0 to +1 while $\coth(x)$ decreases from ∞ to 1. This behavior leads to the following conditions :

$$i. \quad 1 > \beta \geq 0 \quad \dots(16)$$

$$\text{and } ii \quad 1 > a \coth \sqrt{s/\alpha} d \geq 0 \quad \dots(17)$$

The equality represents the case when $h = 0$, i.e., the case of a thermally insulated rear surface [19].

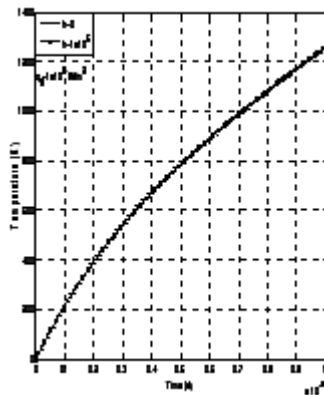


Fig. 7: Ge

$$-\sum_{n=1}^{\infty} (-1)^n \frac{4h}{n^2 \pi^2} \sin \frac{n\pi(d-x)}{d} \exp \left(-\frac{k^2 \pi^2 \alpha t}{d^2} \right) \bar{x}_{n,0} + \sum_{n=1}^{\infty} (-1)^n \frac{4h^2}{(n^2 - k^2) n^2 \pi^2 \alpha} \sin \frac{n\pi(d-x)}{d} \left[\exp \left(-\frac{k^2 \pi^2 \alpha t}{d^2} \right) - \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \right] \quad \dots(18)$$

The temperature of the front surface $T(0,t)$ at $x = 0$ and that of the rear surface at $x=d$ can be easily obtained by substituting $x=0$ and $x=d$ respectively in equation (18).

Using the standard tables of the inverse Laplace transform [24] and taking into consideration the convolution property. One can finally get the required solution in the form :

$$T(x,t) = \left[\frac{q_0 A \cosh \sqrt{s/\alpha} (d-x)}{\lambda s \sqrt{s/\alpha} \sinh \sqrt{s/\alpha} d} \right] \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) - \frac{q_0 A h}{\lambda \rho C_p} \left[\frac{\pi^2}{2 d^2} + \sum_{n=1}^{\infty} \frac{2t}{n^2 \pi^2} - \sum_{n=1}^{\infty} \frac{2d^2}{n^2 \pi^2 \alpha} \left(1 - \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \right) \right] + \sum_{n=1}^{\infty} (-1)^n \frac{2t}{n^2 \pi^2} \cos \frac{n\pi(d-x)}{d} - \sum_{n=1}^{\infty} (-1)^n \frac{2d^2}{n^2 \pi^2 \alpha} \cos \frac{n\pi(d-x)}{d} \left(1 - \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \right) - \left(1 - \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \right) + \sum_{n=1}^{\infty} (-1)^n \frac{4d^2}{n^2 k^2 \pi^2 \alpha} \cos \frac{n\pi(d-x)}{d} \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \bar{x}_{n,0} + \sum_{n=1}^{\infty} (-1)^n \frac{4d^2}{(n^2 - k^2) k^2 \pi^2 \alpha} \cos \frac{n\pi(d-x)}{d} \left[\exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) - \exp \left(-\frac{k^2 \pi^2 \alpha t}{d^2} \right) \right] + \frac{q_0 A h}{\lambda \rho C_p} \left[\frac{(d-x)^2}{d} + \frac{2d^2}{\pi^2} \sum_{n=1}^{\infty} \frac{(-1)^n \sin \frac{n\pi(d-x)}{d}}{n^2} \left(1 - \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \right) \right] - \frac{q_0 A h^2}{\lambda^2 \rho C_p} \left[\frac{\pi(d-x)^2}{2d^2} + \sum_{n=1}^{\infty} \left\{ \frac{2(d-x)}{n^2 \pi^2} - \frac{2(d-x)^2}{n^2 \pi^2 \alpha} \left(1 - \exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) \right) \right\} \right] + \sum_{n=1}^{\infty} \frac{(-1)^n}{n^2} \sin \frac{n\pi(d-x)}{d} \left\{ \frac{2d}{\pi} + \frac{2d^2}{n^2 \pi^2 \alpha} \left(\exp \left(-\frac{n^2 \pi^2 \alpha t}{d^2} \right) - 1 \right) \right\} + \sum_{n=1}^{\infty} (-1)^n \frac{4d^2}{n^2 k^2 \pi^2 \alpha} \sin \frac{n\pi(d-x)}{d} \left(1 - \exp \left(-\frac{k^2 \pi^2 \alpha t}{d^2} \right) \right) -$$

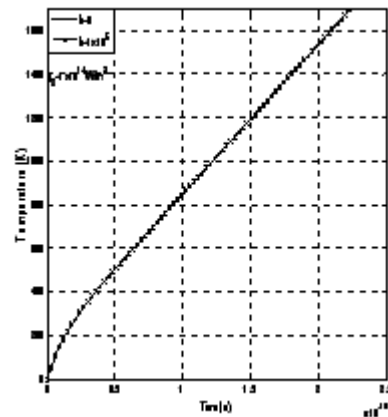


Fig. 8: Si

Computations

As illustrative examples computations are made to obtain the critical time required to initiate melting t_m for the considered elements.

Each target is assumed to be of thickness $d = 5$ mm and is subjected to constant laser flux of irradiance $q_0 = 10^{12}$, W/m² and $q_0 = 1E 14$ W/m². To ensure good cooling conditions high value $h = 10^5$

W/m²K of the heat transfer coefficient is also considered at the rear surface.

The physical and optical parameters of the chosen elements are obtained from refs, 25, 26 and are given in Table 1

The computed values t_m for the considered elements are given in table 2.

CONCLUSIONS

The obtained values for t_m makes it possible to conclude that:

1. Cooling conditions at the rear surface of a target exposed to light of high power density are not effective.
2. The difference in the critical time required to initiate damage for $h=0$ and $h=10^5$ W/m²K is almost undetectable for such sources of high power densities.
3. The values of the critical time required to initiate melting is strongly dependent on the incident power density and the value of the absorption coefficient of the irradiated surface.

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